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# X-Ray Tomography-Based Microstructure Representation in the Snow Microwave Radiative Transfer Model

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**Abstract**—The modular Snow Microwave Radiative Transfer (SMRT) model simulates microwave scattering behavior in snow via different selectable theories and snow microstructure representations, which is well suited to intercomparisons analyses. Here, five microstructure models were parameterized from X-ray tomography and thin-section images of snow samples and evaluated with SMRT. Three field experiments provided observations of scattering and absorption coefficients, brightness temperature, and/or backscatter with the increasing complexity of snowpack. These took place in Sodankylä, Finland, and Weissfluhjoch, Switzerland. Simulations of scattering and absorption coefficients agreed well with observations, with higher errors for snow with predominantly vertical structures. For simulation of brightness temperature, difficulty in retrieving stickiness with the Sticky Hard Sphere microstructure model resulted in relatively poor performance for two experiments, but good agreement for the third. Exponential microstructure gave generally good results, near to the best performing models for two field experiments. The Independent Sphere model gave intermediate results. New Teubner–Strey and Gaussian Random Field models demonstrated the advantages of SMRT over microwave models with restricted microstructural geometry. Relative model performance is assessed by the quality of the microstructure model fit to micro-computed tomography (CT) data and further improvements may be possible with different fitting techniques. Careful consideration of simulation stratigraphy is required in this new era of high-resolution microstructure measurement as layers thinner than the wavelength introduce artificial scattering boundaries not seen by the instrument.

**Index Terms**—Microstructure, microwave scattering, SMRT model, snow, snow microwave radiative transfer (SMRT).

## I. INTRODUCTION

SNOW microstructure knowledge is essential to determine the scattering properties of snow at microwave frequencies. Simulations of microwave scattering are used as the basis for remote sensing of snow mass for water resources and may be used to investigate how the snow mass has changed over the last few decades. The Snow Microwave Radiative Transfer (SMRT) model has recently been developed in order to examine the impact of the representation of the microstructure, to provide consistent theoretical treatment for passive and active simulations, and as a basis for a community model open to future developments [1]. This article provides a thorough evaluation of the SMRT model against observations from three different field campaigns.

Many previous simulations of microwave emission and scattering in the snow using inputs from *in situ* measurements or snowpack evolution model simulations have a common feature: scaling of the microstructure parameters is applied in order to obtain reasonable comparison with observed radiometric data. Scaling has been applied to observations of traditional grain size [2] as used in the Helsinki University of Technology (HUT) model [3], [4], exponential correlation length [5] as used in the Microwave Emission Model of Layered Snowpacks (MEMLS) [6], [7], and sticky hard sphere (SHS) [8] as used by models based on Dense Media Radiative Transfer (DMRT) theory [9]. Stickiness is a secondary (dimensionless) parameter used in the SHS microstructure model and represents the degree of clustering between individual grains. A number of intercomparison studies between these models has illustrated different scaling factors required for each model [10]–[13]. Stickiness itself is a challenging parameter to quantify [14].

Traditional grain size is a notoriously observer-dependent measurement and is largely incompatible with the accuracy requirements for the snow microstructure of around 0.01–0.04 mm [15]. In recent years, new instruments have been developed to measure the snow microstructure in the field from reflectivity measurements at near-infrared wavelengths [16], which gives snow specific surface area (SSA) from which an optical grain diameter can be determined.

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Other methods of determining SSA include gas adsorption, and microcomputed X-ray tomography [17] [micro-computed tomography (CT)]. However, SSA only is insufficient to fully parameterize microstructure models. Micro-CT can provide the missing information because it gives a 3-D reconstruction of the ice-air matrix from which the correlation function may be calculated and the parameters of the analytical correlation functions can be fit to the observed correlation function.

Until recently, microwave scattering models have not kept up to date with the developments in snow microstructure observation techniques. SMRT was developed in part as a response to new instruments, especially micro-CT, but also from a demonstration of the sensitivity to microstructure [15] and a need for more than one microstructure length scale. SMRT was evaluated against a substantial dataset of Arctic and sub-Arctic snow in [18] for SHS and exponential microstructure. The present article is the first to use tomographic microstructure observations to provide an extensive evaluation of the performance of SMRT against field observations for all SMRT microstructure models.

The evaluation is conducted in three steps, with data from three different field campaigns. The first step is a fundamental evaluation of the scattering and absorption coefficients given detailed microstructure information from micro-CT samples acquired during the Arctic Snow Microstructure Experiment (ASMEx) [19]. The second step is an evaluation of a shallow snowpack simulation of brightness temperature with a very simple lower boundary condition, with snowpack correlation functions given by analysis of thin section images acquired with the Passive and Active Microwave and Infrared Radiometer (PAMIR) instrument [20]. The third step is the evaluation of the active portion of the model given a snapshot of the micro-CT profile of a complete snowpack with natural substrate and to present simulations of the angular dependence of both brightness temperature and backscatter. Data are from the Nordic Snow Radar Experiment (NoSREx) [21].

Section II presents a brief description of SMRT. The three field campaigns and the simulation methodology are described in Section III. Results are given in Section IV followed by discussions and conclusions in Sections V and VI.

## II. SMRT MODEL

The SMRT model [1] was developed in response to increased understanding of the importance of microstructure parameterization in snow, and to enable isolation of individual model components in microwave scattering model intercomparison studies. For this, SMRT has a modular structure, which clearly separates the different steps of the calculation (permittivities of the raw materials, scattering coefficients, and solution of the radiative transfer (RT) equation), and for each step offers different theoretical assumptions or theories that can be selected by the user. To facilitate the modular nature, SMRT is written in Python with object-oriented programming techniques and a plugin system. It has been released to the community under an open-source license (see Section VII on code availability) in order to allow it to be used as a general framework for future developments.

For an evaluation of SMRT in this article, correlation functions of the snow were determined from field samples. To focus on the microstructure model approaches, the Improved Born Approximation (IBA) was used as the electromagnetic model for all the simulations in this article. Other theories available in SMRT to compute scattering are specific to a particular microstructure form (e.g., DMRT quasi-crystalline approximation (QCA) is for SHS only). In IBA, the bistatic scattering coefficient (also known as the phase function) is defined for a 2-phase medium (subscript 1 denotes the host constituent and subscript 2 denotes the scattering constituent). Radiation from the direction given by zenith and azimuth angles  $\vartheta', \varphi'$  is scattered into  $\vartheta, \varphi$ , according to [22]

$$p(\vartheta, \varphi, \vartheta', \varphi') = f_2(1 - f_2)(\epsilon_2 - \epsilon_1)^2 Y^2(\epsilon_1, \epsilon_2) M(|\mathbf{k}_d|) k_0^4 \sin^2 \chi \quad (1)$$

where  $f_2$  is the fractional volume of the scattering constituent,  $\epsilon$  is the permittivity,  $Y^2$  is the mean squared field ratio i.e., ratio of the field inside the scattering materials to that incident on it,  $M(|\mathbf{k}_d|)$  is the microstructure function,  $k_0$  is the wavevector in free space and  $\chi$  is the polarization angle. The microstructure function in IBA is determined from the Fourier transform (FT) of the correlation function  $\tilde{C}(|\mathbf{k}_d|)$ , as described by [1], [14].  $\mathbf{k}_d$  is the wavevector difference between scattering and incidence angles and is dependent on the effective permittivity of the medium computed with the Polder–Van Santen mixing formula [23]. For this implementation of SMRT, the simplification of spherical symmetry has been applied for scattering, which means that  $|\mathbf{k}_d|$  can be replaced with  $k_d$ . The microstructure function can then be calculated as

$$M(k_d) = \frac{1}{4\pi} \frac{\tilde{C}(k_d)}{f_2(1 - f_2)}. \quad (2)$$

As with any model, IBA is a theory with limitations. At present, only two constituents may be represented (here, ice and air). To allow an arbitrary arrangement of scattering material within the medium, the propagation speed is assumed constant throughout the snow layer. In this implementation, the relationship between the electric field inside scatterers and that outside is assumed to be the same as for spherical scatterers as this ratio is more dependent on the volume fraction than the type of scatterer [22]. Despite limitations specific to IBA, IBA remains closely related to DMRT theory, at least in the low-frequency limit [14]. DMRT was shown to be limited to small and moderate densities [24], [25], which is likely to apply to IBA, but needs further comparison with exact electromagnetic calculations. SMRT allows a comparison between IBA and DMRT at higher frequencies but is not considered in this article due to the SHS microstructure restriction in DMRT.

For the simulations in this article, five different microstructure models were used: spherical model also known as independent sphere (IND), SHS, exponential (EXP), Teubner–Strey (TS), and Gaussian Random Field (GRF). Analytical expressions for the correlation functions in Fourier space as required by (2) exist for all but the GRF model.  $\tilde{C}(k_d)$  for the SHS model, which requires sphere radius and stickiness as

parameters, was given in 31 of [14]. The microstructure functions in Fourier space for the IND, EXP, and TS models are

$$\tilde{C}_{\text{IND}}(k) = f_2(1 - f_2) \left( \frac{\pi d_{\text{ind}}^3}{6} \right) \left[ \frac{3(\sin X - X \cos X)}{X^3} \right]^2 \quad (3)$$

$$X = k_d d_{\text{ind}}/2$$

$$\tilde{C}_{\text{EXP}}(k_d) = \frac{8\pi l_{\text{ex}}^3 f_2(1 - f_2)}{[1 + (k_d l_{\text{ex}})^2]^2} \quad (4)$$

$$\tilde{C}_{\text{TS}}(k_d) = \frac{8\pi \zeta_{\text{TS}}^3 f_2(1 - f_2)}{[1 + Z]^2 + 2[1 - Z](k_d \zeta_{\text{TS}})^2 + (k_d \zeta_{\text{TS}})^4}$$

$$Z = \left( \frac{2\pi \zeta_{\text{TS}}}{d_{\text{TS}}} \right)^2 \quad (5)$$

where  $d_{\text{ind}}$  is the IND diameter,  $l_{\text{ex}}$  is the exponential correlation length,  $\zeta_{\text{TS}}$  is the TS correlation length and  $d_{\text{TS}}$  is the TS domain length (also known as repeat distance).

For GRF, numerical calculation of the FT of the correlation function has been applied as an analytical form cannot be found. The GRF real space correlation function (as a function of distance  $r$ ) is given as

$$C_{\text{GRF}}(r) = f_2(1 - f_2) \frac{1}{2\pi} \int_0^{C_v(r)} \frac{1}{\sqrt{1-t^2}} \exp\left[-\frac{\beta^2}{1+t}\right] dt \quad (6)$$

where  $\beta$  is a cut-level parameter ([26]) related to the volume fraction. The correlation function of the underlying random field currently used for the GRF in SMRT is

$$C_\psi(r) = \exp(-r/\zeta_{\text{grf}}) \left( 1 + \frac{r}{\zeta_{\text{grf}}} \right) \frac{\sin(2\pi r/d_{\text{grf}})}{(2\pi r/d_{\text{grf}})} \quad (7)$$

where  $\zeta_{\text{grf}}$  is the GRF correlation length and  $d_{\text{grf}}$  is the GRF domain length (or repeat distance).

The RT solver in SMRT is based on the Discrete Ordinates (DORT) approach with stream matching at the boundaries as described in [1]. Fourier decomposition is used to deal with the azimuthal dependence of the phase function and allows computation of the general solution of the RT equations by eigenanalysis, while the particular solution is obtained by solving a linear system representing the boundary conditions. So, it is the FT of the IBA phase function with respect to the azimuthal component that is used by the solver. The evaluation is done numerically.

Section III describes the three field campaigns with sufficient microstructural data to evaluate SMRT for all implemented microstructure models. Each dataset and simulation methodology are described in turn.

### III. EVALUATION DATA DESCRIPTION AND METHODS

Fitting of the microstructure models to the micro-CT data followed a common procedure for all datasets. This is described in Section III-D, after the descriptions of individual field experiments.

#### A. Arctic Snow Microstructure Experiment (ASMEx)

The ASMEx [19] took place in Sodankylä, Finland in the winters of 2013–2014 and 2014–2015. This field campaign

was specifically designed to measure scattering and absorption coefficients of slabs of homogeneous snow in order to develop a new snow extinction coefficient model as a function of SSA for the HUT snow emission model [4], [27]. Data from this campaign included micro-CT samples and therefore provide an ideal dataset to evaluate the SMRT microstructure and electromagnetic components of the model independently of the solver. This section provides a brief description of the field measurement methodology, retrieval of scattering and absorption coefficients, and simulation approach. A total of 14 horizontal snow slabs (width = 60 cm, length = 80 cm, various heights) were extracted and observed with microwave radiometers during the ASMEx field campaign.

Brightness temperatures ( $T_B$ )s of the snow slabs were measured on 1) a metal (highly reflecting) base and 2) microwave absorber (highly absorbing) base [27] at frequencies of 18.7, 21, 36.5, 90, and 150 GHz. A metal sheet was used to transfer the snow slab from the natural snowpack onto microwave absorbers where the metal base observations were made. The metal sheet was then carefully slid from under the snow slab to allow the snow slab to rest on the microwave absorber, as described in [19]. Measurement error specification for these instruments is 1 K, independently confirmed for 18.7–90 GHz by [21]. For ASMEx, the measurement protocol was similar in each case, with minor differences in absorber material used and frequency range observed due to equipment availability, as described in [28]. Destructive sampling of the snow slabs was then carried out roughly in order from least destructive to most destructive as described by [28]. Snow micropenetrator profile measurements were taken first, followed by temperature, density then SSA profiles within the slab. Snow grain macro photographs were also taken after SSA observations. Finally, two samples of cross section 5 cm × 5 cm (height of slab governs the third dimension, typically around 15 cm) were taken [28], one from the radiometer center of field of view and another in close proximity. These samples were cast in di-ethyl pththalate in the field, transported to the WSL Institute for Snow and Avalanche Research SLF in Davos, Switzerland, where they were processed and observed with an X-ray microtomography (micro-CT) instrument.

A total of 14 slabs were observed over the two winter seasons: slabs A01-A07 in the first season and slabs B01-B07 in the second. The orientation of micro-CT samples from slab A01 differed from the remaining slabs as horizontal rather than vertical profiles were taken, and only one cast sample was taken for slab A02 (for calculation of error statistics, the second A02 sample was assumed to be the same as the first). Cylindrical sections were extracted from the vertically casted snow samples and cut in half in order to fit into the micro-CT instrument, as illustrated by Fig. 1. This means that a small section of snow is missing due to the thickness of the saw, although this gap is neglected for analysis purposes. Snow parameters were then determined for smaller overlapping cubic subsamples within each micro-CT sample.

Snow density and SSA were calculated from 120 voxel height subsamples, which corresponds to a subsample height of 2.18 mm. Mean density and SSA for each of the slab is shown in Fig. 2. Although the slabs were visually

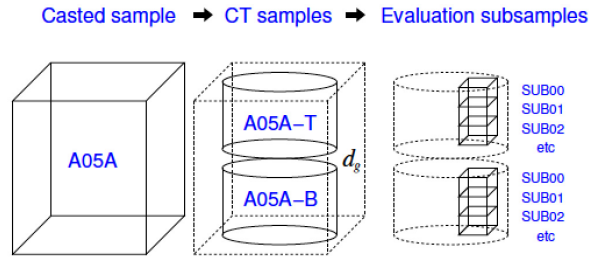


Fig. 1. Processing of slab samples (except slab A01): Slab samples were sliced into two micro-CT samples, and scanned with a nominal resolution (voxel size) of  $18 \mu\text{m}$ . Microstructure parameters were calculated over  $10.8 \text{ mm}$  stacked, overlapping subsamples.

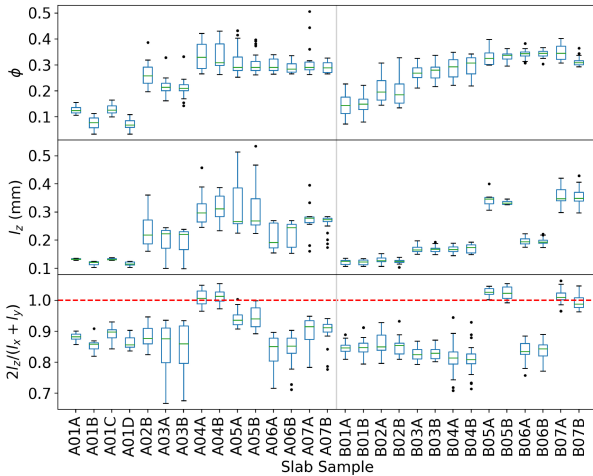


Fig. 2. Microstructure properties for 14 ASMEEx slab subsamples. Gray line separates samples taken in two different seasons. (Top) Fractional volume of ice. (Middle) Correlation length in vertical direction. (Bottom) Ratio of vertical correlation length to horizontal correlation length (anisotropy).

homogeneous at the point of extraction, the density and SSA range within each slab show that they are not strictly homogeneous. Early in the season (lower slab samples) the slabs are characterized by lower density and smaller microstructure scales/sizes; both generally increase as the season progresses. Perfectly isotropic snow would have equal horizontal and vertical correlation lengths i.e., anisotropy factor  $2 \ell_z/(\ell_x + \ell_y) = 1$  as shown by the red dashed line in Fig. 2. An anisotropy factor of less than 1 means the correlation length is larger in the horizontal direction than the vertical, which is the case for the majority of slab samples, as expected for surface snow that has hardly undergone any temperature gradient metamorphism [29]. The microstructure is larger in the vertical for slabs A04, B05, and B07 only. Spherical symmetry is assumed in the version of SMRT used in this article, which may not be appropriate and is discussed later in this article.

Correlation functions of the snow were determined from the 3-D structure of the ice matrix and parameters retrieved for the five analytical correlation function models by minimization of the cost function (further details given below). A summary of microstructure parameters for all slabs is given in Table I.

Density and microstructure parameters were used to calculate scattering and absorption coefficients for each micro-

TABLE I

SUMMARY OF MICROSTRUCTURAL PROPERTIES FOR ALL THREE EXPERIMENTS (IQR IS INTERQUARTILE RANGE). ASMEEX AND NOSREX PARAMETERS WERE DERIVED FROM MICRO-CT DATA, PAMIR PARAMETERS WERE DERIVED FROM THIN SECTION IMAGES. DENSITY IS GIVEN IN  $\text{Kg m}^{-3}$ ,  $\tau$  IS DIMENSIONLESS, ALL OTHER MICROSTRUCTURAL PARAMETERS ARE GIVEN IN  $\text{mm}$ . ASMEEX, PAMIR AND NOSREX DATASETS HAVE 562, 10 AND 320 SUBSAMPLES, RESPECTIVELY

|             | ASMEEx |      | PAMIR  |      | NoSREx |      |
|-------------|--------|------|--------|------|--------|------|
|             | Median | IQR  | Median | IQR  | Median | IQR  |
| Density     | 258    | 95   | 397    | 66   | 217    | 87   |
| $d_{SHS}$   | 0.50   | 0.38 | 0.80   | 0.38 | 0.15   | 0.16 |
| $\tau$      | 0.10   | 0.12 | 0.10   | 0.05 | 0.11   | 0.02 |
| $l_{ex}$    | 0.14   | 0.09 | 0.46   | 0.12 | 0.11   | 0.15 |
| $d_{IND}$   | 0.41   | 0.28 | 1.23   | 0.31 | 0.32   | 0.44 |
| $\xi_{TS}$  | 0.20   | 0.13 | 0.53   | 0.15 | 0.14   | 0.19 |
| $d_{TS}$    | 1.46   | 2.67 | 502    | 340  | 2.21   | 333  |
| $\xi_{GRD}$ | 0.14   | 0.10 | 0.37   | 0.11 | 0.10   | 0.14 |
| $d_{GRF}$   | 1.70   | 33)  | 485    | 333  | 8.12   | 334  |

CT subsample to evaluate SMRT scattering theories independently of other SMRT modules (namely the RT solver, substrate, atmosphere, and interface modules). Simulations of the absorption and scattering coefficients were carried out for all slab subsamples at all ASMEEx frequencies for all five microstructure models. Slab means of these subsample coefficients were compared against the bulk slab coefficients retrieved from the radiometric data by [27]. As described in [27], there is a difference between coefficients retrieved from horizontally and vertically polarized observations. Here, the mean of the coefficients derived at both polarizations is used as the observations for comparison with SMRT.

For calculation of  $T_B$ , the slabs were reconstructed from the micro-CT subsamples with one snowpack layer corresponding to one micro-CT subsample with layer thickness scaled to account for mass lost during micro-CT preparation. For the simulations, the substrate was assumed to be a perfect reflector for the metal plate case, whereas for the absorber substrate, the reflectivity was determined from the measured emissivity. Where absorber emissivity observations were not available, the mean of all observations at that frequency was used. Measured downwelling atmospheric  $T_B$  was used to parameterize the simple isotropic atmosphere in SMRT (a single plane parallel layer that follows MEMLS formulation [30]) and included in simulation of  $T_B$ .

### B. Passive and Active Microwave and Infrared Radiometer (PAMIR) Snow Crust Experiment

The PAMIR system included five microwave radiometers at frequencies 4.9, 10.4, 21, 35, and 94 GHz (measurement error  $\sim 1 \text{ K}$  at 260 K [31]) mounted on a 15 m tower at an incidence angle of  $50^\circ$  at the Weissfluhjoch, Davos site from 1977 to 1987. Here, we describe a snow crust experiment that took place 8–10 May 1984 when the snowpack underwent two melt-refreeze cycles. The depth of refrozen snow was measured manually and the snowpack observed with PAMIR over the course of the experiment (33 measurements over 41 h) [20] and two thin section images were taken, shown in Fig. 3.

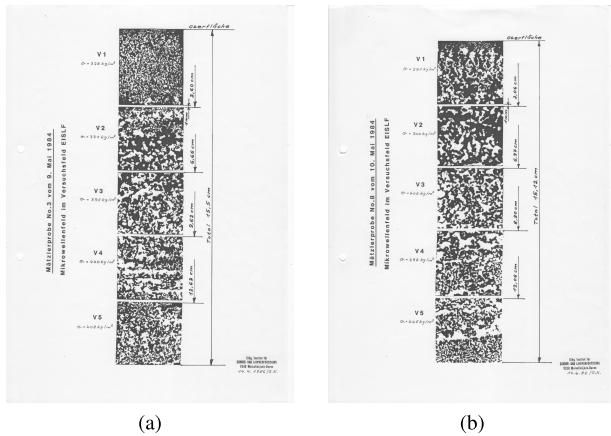


Fig. 3. Thin section images from PAMIR melt-refreeze experiment. (a) May 9, 1984. (b) May 10, 1984.

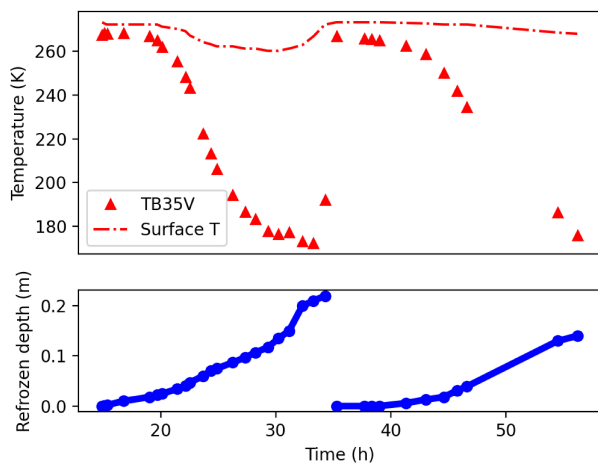


Fig. 4. Time series of refrozen snow depth (blue), surface temperature (red dot-dashed line) and observed brightness temperature at 35 GHz, vertical polarization (red triangles) for the PAMIR snow crust experiment, May 8–10, 1984.

Correlation functions were calculated in the  $z$ - and  $x$ -direction for each of the five subsections in both images and together with the layer thickness and density observations noted in the images were used to construct a time series of snowpacks of depth given by the refrozen thickness measurements shown in Fig. 4. Also shown in Fig. 4 is the decrease in surface temperature and snowpack brightness temperature at 35 GHz as the snowpack refreezes, with a sudden reversal as the snowpack returns to a melting state. Table I gives a summary of the analytical microstructure model parameters derived from the thin section images, averaged over horizontal and vertical directions, where the  $y$ -direction parameters are assumed to be the same as in the  $x$ -direction.

These microstructural parameters were used to construct numerical snowpacks of time-dependent depth and assumed lower boundary emissivity of 96% at 0 °C. Sky  $T_B$  observations were used to parameterize a simple isotropic atmosphere, which was included in the simulations. The temperatures of the snow layer midpoints were calculated by linear interpolation between the melt interface at 0 °C and the observed

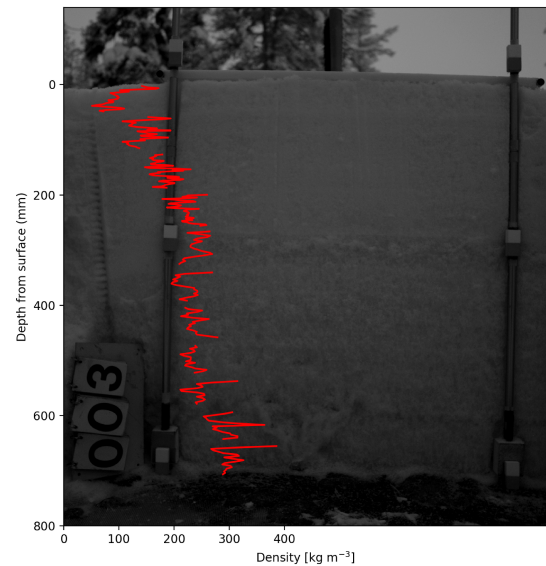


Fig. 5. NoSREx density derived from micro-CT samples overlaid on image of snowpit face. Sample taken on Mar. 1, 2012.

temperature at the snow surface. These data were used to drive SMRT simulations and were compared to the time series of passive data from the snow crust experiment (active data were not available for comparison).

### C. Nordic Snow Radar Experiment (NoSREx)

The NoSREx took place in Sodankylä, Finland over four winter seasons and is described fully in [21]. The simulations presented here focus on the third season (2011–2012) where a near-complete micro-CT profile was available. Angular observations ( $30^\circ$ – $60^\circ$ ) of both  $T_B$  and backscatter ( $\sigma_0$ ) are available for this campaign, and thus provides the first test of SMRT in active mode. An array of radiometers (V and H 10.65, 18.7, 21, 36.5 GHz) was installed on a tower 4.1 m above ground and a four-polarization scatterometer operating between 9.2 and 17.9 GHz was mounted 9.6 m above ground nearby. As with ASMEx, brightness temperature measurement error for 18.7–36.5 GHz radiometers is 1 K. Measurement error at 10.65 GHz is 2 K due to the radiometer design [21]. Backscatter measurement error is of the order 1 dB [21].

Fig. 5 illustrates the non-continuous density profile determined from micro-CT data. For simulation of a continuous snowpack, layers were constructed from each available micro-CT subsample and constant layer thickness derived from the automated sensor snow depth. The temperature profile of the snowpack was estimated by linear interpolation between automated measurements of the air temperature and 2 cm below the soil surface (mean of observations at two locations) limited to a maximum of 0 °C. A summary of the microstructural parameters over this profile is given in Table I.

For the passive simulations, soil reflectivity was calculated with [32], assuming a soil roughness root mean square height of 2 cm. The soil permittivity was determined from the mean of two soil moisture measurements at 2 cm depth, soil sand content of 70%, clay content of 1% and dry density

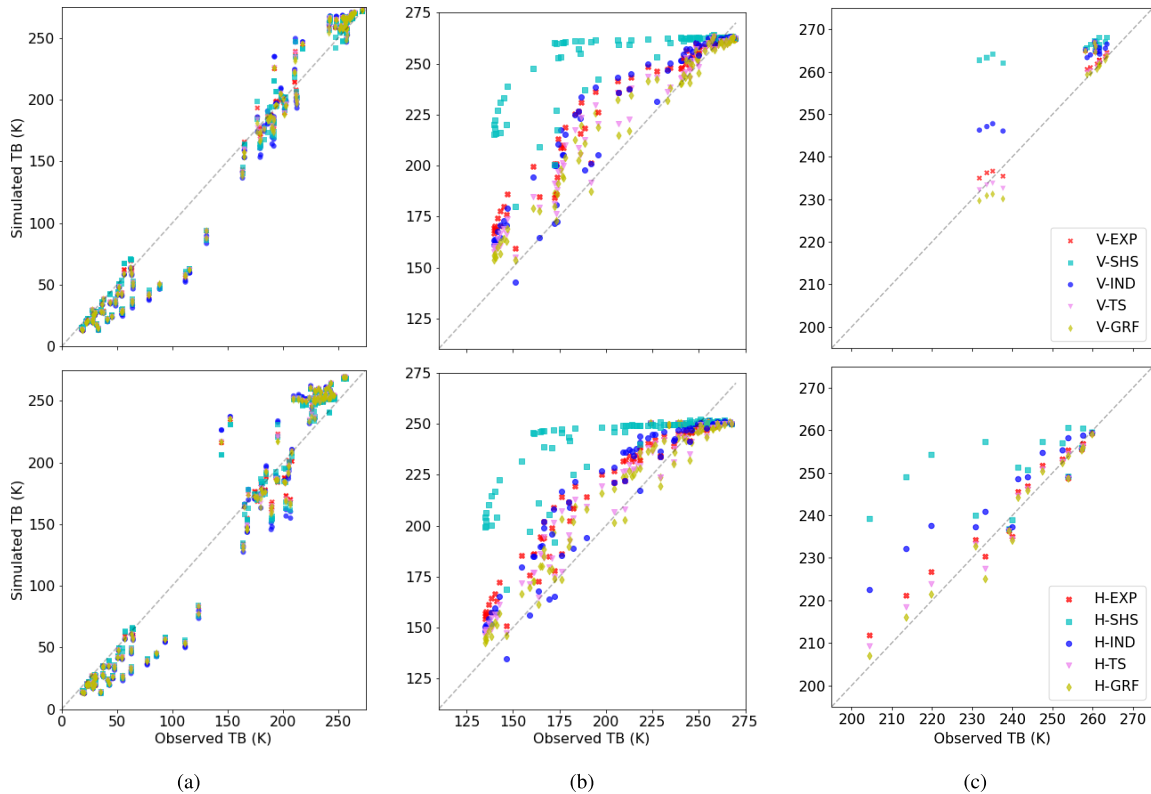


Fig. 6. Scatterplot comparison between observed and simulated brightness temperature (all frequencies observed, all incidence angles. V-polarization shown on top graphs, H-polarization shown on bottom. (a) ASMEEx. (b) PAMIR. (c) NoSREx.

of  $1300 \text{ kg m}^{-3}$  with the model of [33]. The atmospheric contribution was approximated with nadir observations applied to the SMRT simple isotropic atmosphere, which will result in a small underestimation in  $T_B$  as a function of incidence angle. Rather than overfitting the soil contribution in the absence of data, a soil backscatter of  $-13 \text{ dB}$  was assumed to be a reasonable approximation for both HH and VV polarization. For active simulations, micro-CT subsample layers were aggregated in groups of 20 so that the snowpack of 76 cm depth was represented by 16 layers for frequencies of 10.2, 13.3, and 16.7 GHz.

#### D. Microstructure Parameter Fitting

Similar to all datasets, the parameters for the SMRT microstructure models were obtained by fitting the auto-correlation functions obtained from binary 3-D micro-CT images (NoSREx, ASMEEx) or 2-D binary thin sections images [PAMIR, cf. Fig. 3(a)]. All fits were done by using MATLAB's `lsqnonlin` optimization over a fixed number of data points (100) and allowing for a global normalization prefactor. The ice volume fraction (density) was obtained directly by counting the ice voxels/pixels of the images. The real space models (EXP, IND, TS, GRF) were fit along the main coordinate directions ( $x, y, z$ ) of the 3-D/2-D correlation function yielding direction-dependent parameters that were subsequently averaged (arithmetic mean over directions) to obtain a single set of parameters for an isotropic model. For the

isotropic Fourier model (SHS) the 3-D FT of the correlation function was spherically averaged and subsequently fit.

## IV. SMRT EVALUATION RESULTS

### A. Brightness Temperature

Brightness Temperature ( $T_B$ ) observations were available for all field campaigns. Fig. 6 shows scatterplot comparisons between observed and simulated brightness temperature for each snow microstructural model and for each field campaign over all available frequencies. The ASMEEx campaign observations in Fig. 6(a) cover a wider  $T_B$  range than PAMIR and NoSREx data due to the bottom boundary condition and shallow depth of snow: low  $T_B$  observations are of slabs on top of the metal plate and high  $T_B$  were observed after the plate had been removed and the snow was on top of the microwave absorbing material. The range of  $T_B$  measured in the PAMIR and NoSREx campaigns is smaller but is more representative of observations over natural snowpacks. The microstructure model appears to have only a small influence on the simulated  $T_B$  of the ASMEEx slabs. Low  $T_B$  tends to be underestimated and high  $T_B$  overestimated for ASMEEx. Outliers in the central range of observed values (approximately 100–150 K) were slabs A02, A04, and B07 at either 21 or 36.5 GHz.  $T_B$  at other frequencies for these slabs are more closely grouped with  $T_B$  of other slabs.

PAMIR data in Fig. 6(b) show a wide range of simulated  $T_B$  for a given observation e.g., an observed H-pol  $T_B$  of 175 K is represented by simulations over a range of 170–250 K.



TABLE II  
BRIGHTNESS TEMPERATURE ME AND ROOT MEAN SQUARE  
ERROR (RMSE) [K]. SMALLEST ERRORS FOR EACH  
POLARIZATION ARE SHOWN IN BOLD FOR  
EACH FIELD EXPERIMENT

|      |        | EXP | SHS         | IND         | TS   | GRF        |             |
|------|--------|-----|-------------|-------------|------|------------|-------------|
| ME   | ASMEx  | H   | 0.5         | <b>0.2</b>  | -0.3 | -0.2       | -0.3        |
|      |        | V   | <b>-3.0</b> | -3.2        | -4.0 | -3.7       | -3.9        |
|      | PAMIR  | H   | 6.5         | 18.8        | 5.5  | 3.3        | <b>2.1</b>  |
|      |        | V   | 7.3         | 18.9        | 6.2  | 4.0        | <b>2.8</b>  |
|      | NoSREx | H   | 1.3         | 10.6        | 5.3  | <b>0.2</b> | -0.6        |
|      |        | V   | 2.2         | 11.3        | 6.2  | 1.2        | <b>0.3</b>  |
| RMSE | ASMEx  | H   | 22.7        | <b>22.2</b> | 25.1 | 23.3       | 23.2        |
|      |        | V   | 15.3        | <b>15.0</b> | 17.5 | 15.5       | 15.4        |
|      | PAMIR  | H   | 15.2        | 35.1        | 14.5 | 11.6       | <b>10.4</b> |
|      |        | V   | 16.6        | 37.0        | 15.3 | 11.9       | <b>10.2</b> |
|      | NoSREx | H   | 4.3         | 17.1        | 9.0  | 3.6        | <b>3.4</b>  |
|      |        | V   | 3.2         | 15.1        | 7.3  | <b>3.1</b> | 3.6         |

Simulated  $T_B$  are generally overestimated except at high  $T_B$ . However, the SHS microstructure model generally overestimates  $T_B$  by the largest amount. This is also the case for the NoSREx data in Fig. 6(c).

Given the more complicated structure of the full NoSREx snowpack, Fig. 6(c) highlights the overall importance of the microstructure model, particularly at lower  $T_B$ . For the NoSREx dataset, in general, the SHS model gives the highest  $T_B$ , followed by IND, EXP, TS, and with GRF giving the lowest  $T_B$ . A high SHS followed by EXP, TS, GRF in decreasing  $T_B$  order is also apparent in the PAMIR dataset, although IND can be above or below EXP, or have the lowest  $T_B$  of all microstructure models. In contrast, there is no consistency between the relative  $T_B$  given by different microstructure models in the ASMEx dataset: the order changes even for different micro-CT samples of the same slab.

Table II shows the mean error (ME) and root mean squared error (RMSE) for  $T_B$  simulated for each experiment. ME range from  $-4.0$  to  $0.5$  K for ASMEx,  $2.1$  to  $18.9$  K for PAMIR and  $-0.6$  to  $11.3$  K for NoSREx. RMSE ranges from  $15.0$ – $25.1$  K for ASMEx,  $10.2$ – $37.0$  K for PAMIR and  $3.1$ – $17.1$  K for NoSREx. For the ASMEx field campaign, RMSE is the smallest for the SHS, with the smallest ME for SHS (H-pol), TS (H-pol), and EXP (V-pol) microstructures. In contrast, SHS performs poorly for both PAMIR and NoSREx experiments, with the largest ME and RMSE. For PAMIR and NoSREx experiments, TS and GRF microstructure models have the lowest ME and RMSE at both polarizations. The following subsections evaluate each field experiment, in turn, to explore these results further.

### B. Scattering and Absorption Coefficients (ASMEx)

ASMEx data allow evaluation of SMRT absorption and scattering coefficients against those derived in [27], as shown in Figs. 7 and 8. A complete dataset is only available at 21 GHz due to instrumentation failure/installation dates at other frequencies. Calculation of the absorption coefficient ( $\kappa_a$ ) in SMRT IBA is independent of microstructure model so Fig. 7 compares simulated  $\kappa_a$  (mean of subsamples) with observed  $\kappa_a$  for a single microstructure model. Note that  $\kappa_a$  in Fig. 7 have been scaled by  $1/\text{wavenumber}$  to eliminate the direct

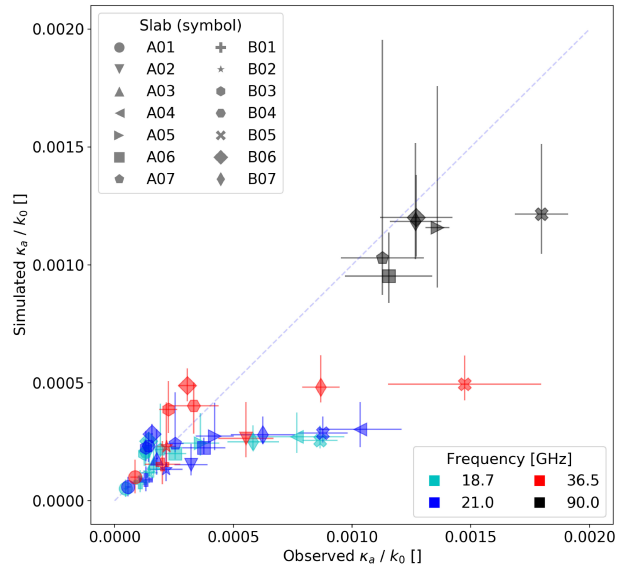


Fig. 7. Scatterplot of ASMEx subsample absorption coefficient, compared with observed absorption coefficient derived from observations in [27]. Coefficients have been normalized with respect to the wavenumber in free space,  $k_0$ . Note that the absorption coefficient is independent of the microstructure model. Observation error bars illustrate the difference between retrievals derived from H- and V-pol observations. Simulation error bars show the range of subsample absorption coefficients relative to the mean.

frequency dependence (an indirect dependence through the permittivity remains). In general, there is a good overlap with the 1:1 line, with a few noticeable outliers: slabs A02, A04, B05, and B07. Slab B05 (shown by crosses) was observed at all frequencies and its  $\kappa_a$  was consistently underestimated in the simulations. At 36.5 GHz,  $\kappa_a$  for slabs A02 (downward triangle) and B07 (thin diamond) were also underestimated, although slab B07 was simulated well at 90 GHz (A02 was not measured at this frequency). At 18.7 and 21 GHz,  $\kappa_a$  for slabs A04 (leftward triangle) and B07 were also underestimated. Comparing  $\kappa_a$  with observations for all slabs, the regression coefficient  $r^2 = 0.94$ , with RMSE of  $0.3 \text{ m}^{-1}$  and ME of  $-0.2 \text{ m}^{-1}$ .

Unlike  $\kappa_a$ , scattering coefficients ( $\kappa_s$ ) depend on microstructure model, as shown in Fig. 8. Note that  $\kappa_s$  has been shown on logarithmic axes. The comparison between models shows that for the ASMEx parameters, EXP, GRF, and TS models give near-identical results and there is also a high agreement between these models and IND. Lower regression coefficients were found between SHS and any other microstructure model, which reflect the increased scatter in SHS  $\kappa_s$ . For comparison with observations, the mean of subsample  $\kappa_s$  was compared with  $\kappa_s$  observed for the entire slab. Across all slabs,  $\kappa_s$  is generally overestimated at 90 GHz but underestimated at 36.5 GHz and below, with larger errors for lower scattering coefficients. This is not unexpected as observation errors and deficiencies in retrieval technique will have the greatest impact where the least scattering occurs. It is, however, difficult to apportion the discrepancies either to the frequency-dependence of IBA or to retrieval errors. Despite these differences, observations and simulations are highly correlated. Lowest  $r^2$  between observed and simulated  $\kappa_s$

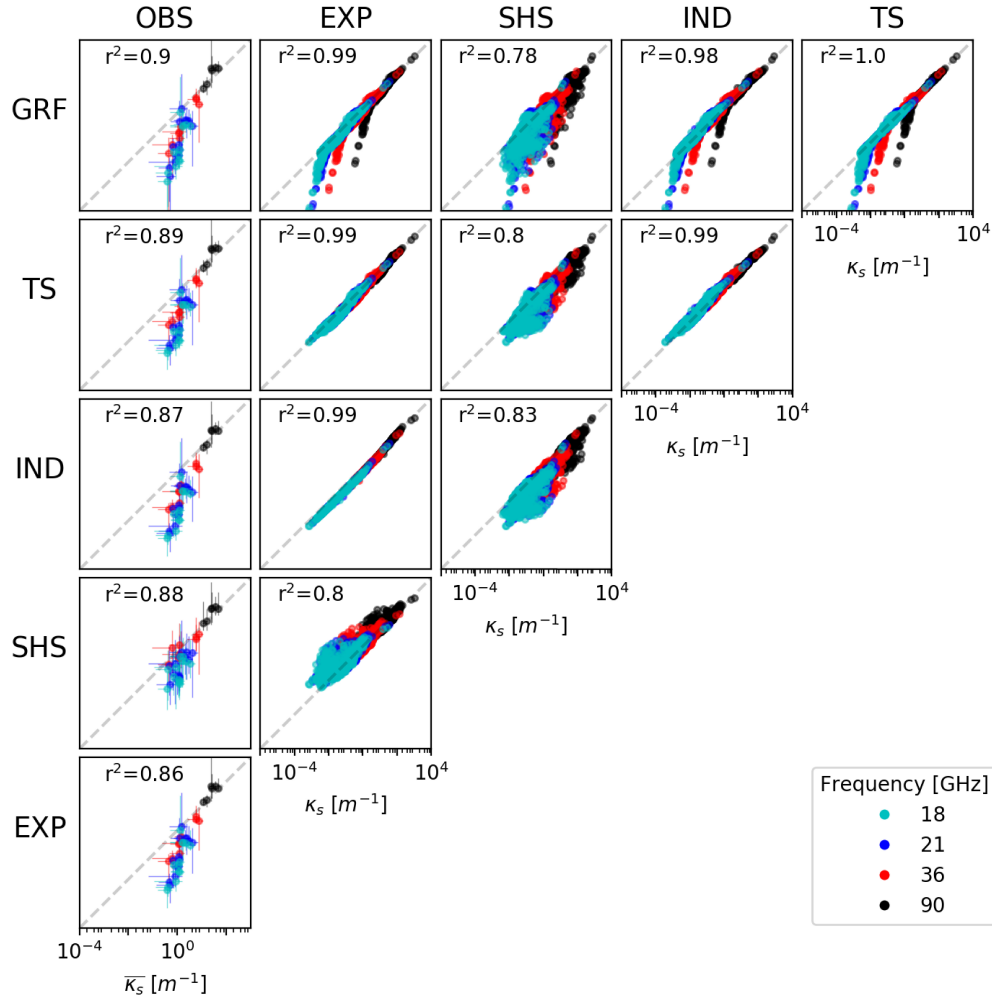


Fig. 8. Scatterplot comparison between scattering coefficients of different microstructure models from ASMEEx subsamples, and a comparison of mean slab scattering coefficients with observed scattering coefficients from [27]. Gray dashed 1:1 line shown. As for Fig. 7, observation error bars illustrate the difference between retrievals derived from H- and V-pol observations. Simulation error bars show the range of subsample absorption coefficients relative to the mean.

occurred for the single length scale models EXP (0.86) and IND (0.87), median  $r^2$  for SHS (0.88), and highest  $r^2$  for the TS (0.89) and GRF (0.9) models. The difference between microstructure model correlation with observations suggests a choice of microstructure model influences the frequency dependence of IBA.

Errors in ASMEEx  $T_B$  can be explained by  $\kappa_s$  at high  $T_B$  and  $\kappa_a$  at low  $T_B$ . At frequencies of 36.5 GHz and below, scattering coefficients are generally underestimated when compared with the retrieved values, which can explain overestimation of  $T_B$  at high  $T_B$  for the ASMEEx data as there is a less simulated scattering of the radiation emitted from the absorber. For low  $T_B$ , where the substrate was a metal plate, differences in  $\kappa_s$  cannot explain the general underestimation in  $T_B$ . Outliers at these low  $T_B$  are generally for slabs A02, A04, B05, and B07, where  $\kappa_a$  and therefore the emission from the snow itself was underestimated. These particular slabs also formed outliers in the central range of ASMEEx  $T_B$ . It is worth noting that slab B05 was considerably thinner (5.4 cm thickness) than other slabs ( $\sim 15$  cm), which may have impacted the accuracy of retrieved  $\kappa_a$  and  $\kappa_s$  for that slab. Less accurate retrievals of

$\kappa_a$  and  $\kappa_s$  can be expected where scattering is low and could partially explain the underestimation of low  $\kappa_s$  in Fig. 8.

Vertical structures within snow assumed to be spherically isotropic resulted in higher  $T_B$  errors than for horizontal structures. Whilst ASMEEx slabs were nominally selected for homogeneity within layers, this was not necessarily the case. In addition, analysis of correlation functions in  $x$ -,  $y$ -, and  $z$ -directions showed that the slabs were anisotropic (Fig. 2). Most of the slabs had an anisotropy factor  $< 1$ , meaning greater correlation lengths in the horizontal than in the vertical. Only slabs A04, B05, and B07 showed anisotropy factors generally  $> 1$  i.e., larger correlation lengths in the vertical direction more commonly associated with vertical features such as depth hoar chains. Scattering and absorption coefficients and brightness temperature for these slabs were less well simulated than for other slabs.

### C. Simple Snowpack (PAMIR)

Whilst Fig. 6(b) gives an overall picture of  $T_B$  simulations for a shallow refrozen snowpack with simple lower boundary condition, Fig. 9 examines the evolution of  $T_B$  over time as

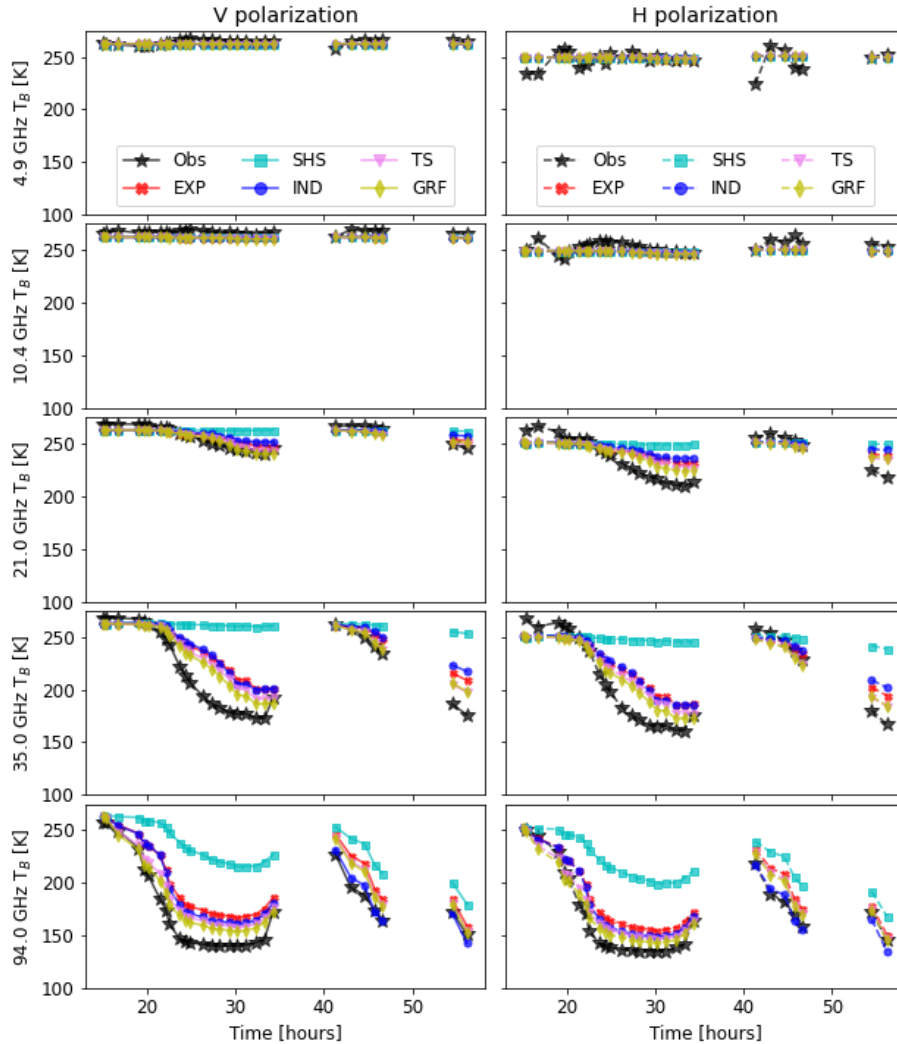


Fig. 9. Time series of brightness temperature for PAMIR experiment (periods with dry surface snow shown).

the snowpack refreezes. At 4.9 and 10.4 GHz, the impact of the snow—and therefore of the microstructure models—is small. There is more variability in the H-pol observations than at V-pol, but the simulations do not capture the observed variability in H-pol  $T_B$ . At higher frequencies, the contribution of the snow increases and the impact of the substrate diminishes. Simulations reflect the rapid decline in observed  $T_B$  with increasing depth of refrozen snow at 21 GHz and above although the observed rate at 35 GHz is faster than simulated. For much of the time series, the GRF model demonstrates the best agreement with observations. The SHS microstructure model does not show good agreement with observations at 21 and 35 GHz but is better able to capture the decline in  $T_B$  at 94 GHz for the second refreeze period. The difference in performance between models is shown in the ME in Table II, with TS and GRF demonstrating the lowest errors.

PAMIR is an ideal dataset for exploring reasons for different microstructure model performances as it is relatively small and there are large differences between microstructure models. Fig. 10 demonstrates how the correlation functions for different microstructure models, as used in SMRT after averaging, compare with observed correlation functions. Data for the

9th May have been shown as continuous  $T_B$  are available for this day. The dominant horizontal (crust) features evident in Sections 2–4 of Fig. 3(a) are reflected by the anisotropy in the real-space correlation function in Fig. 10, with high correlations in the  $x$ -direction tail. Section 5 has vertical features (high correlation in the  $z$ -direction tail) whereas Section I is relatively isotropic. The parameterized correlation functions thus always represent a compromise between the different coordinate directions.

For the real-space correlation functions it is possible to compare their performance via naive fit metrics (mean square error) which are shown in Table III. IND microstructure is the least-well fit microstructure parameter yet  $T_B$  errors in Table II are overall lower than for EXP. However, errors depend on frequency. At 21 GHz, Fig. 6(b) shows higher  $T_B$  errors with IND than EXP, but lower errors at 35 GHz and above. At small scales (e.g.,  $r \lesssim 1$  mm), the IND correlation function shown in Fig. 10 is higher than EXP and TS real-space microstructure models for Sections II–V, indicating more scattering. At larger scales, the lower IND correlation however would suggest less scattering than for other models. In Fourier space, smaller length scales (wavelengths) correspond to larger frequencies.

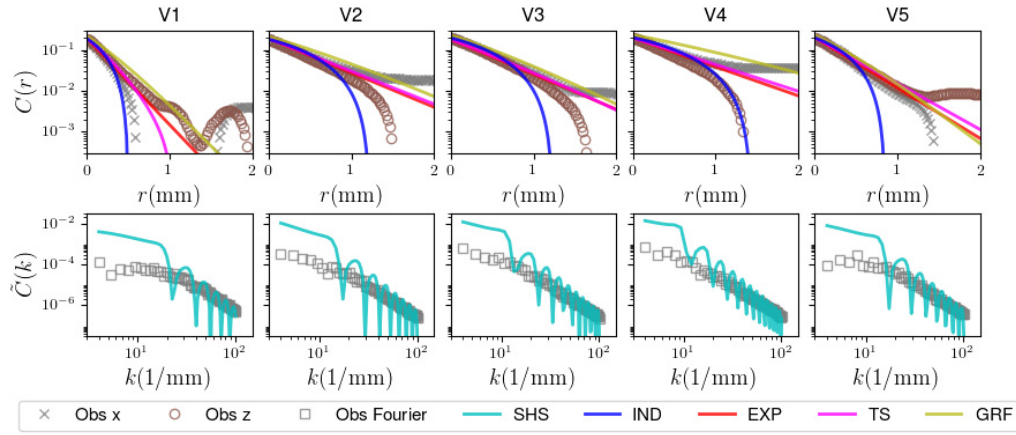


Fig. 10. Comparison between observed and parameterized correlation functions for EXP, IND, TS and GRF in real space (top) and SHS in Fourier space (bottom).

TABLE III

REAL-SPACE FIT METRICS IN  $x$ - AND  $z$ -DIRECTIONS FOR 9TH MAY PAMIR MICROSTRUCTURAL PARAMETERS, CALCULATED AS THE SUM OF THE SQUARED RESIDUALS OF THE NON-LINEAR FIT (*nonlinsq* MATLAB FUNCTION) OVER 100 DATA POINTS (MULTIPLIED BY  $10^3$ ). SHS IS EXCLUDED AS IT MUST BE FIT IN FOURIER SPACE AND IS NOT COMPARABLE

| Layer   | IND  |     | EXP  |     | TS   |     | GRF  |     |
|---------|------|-----|------|-----|------|-----|------|-----|
|         | $x$  | $z$ | $x$  | $z$ | $x$  | $z$ | $x$  | $z$ |
| 1 (top) | 1.6  | 3.5 | 2.2  | 0.3 | 0.6  | 0.3 | 0.6  | 0.3 |
| 2       | 20.2 | 4.6 | 3.9  | 1.7 | 3.9  | 0.6 | 5.0  | 0.7 |
| 3       | 8.5  | 3.6 | 0.4  | 1.8 | 0.4  | 0.1 | 0.6  | 0.2 |
| 4       | 37.1 | 8.6 | 13.1 | 9.5 | 13.1 | 4.3 | 15.1 | 3.9 |
| 5       | 3.6  | 8.5 | 0.8  | 1.6 | 0.3  | 1.6 | 0.4  | 2.1 |

IND could have lower  $T_B$  errors than EXP at higher frequencies because of the poor but higher fit at small scales. IND correlation underestimation at larger scales is more relevant at lower frequencies and could explain why  $T_B$  is higher for IND than any other real-space microstructure model at low frequencies.

TS is a better fit to the measured correlation than EXP (although demonstrates EXP-behavior in the  $x$ -direction for Sections II–IV). The correlation is also higher than EXP at all scales. The larger TS scattering leads to lower  $T_B$  errors. GRF correlations are generally higher than TS, resulting in further reductions in  $T_B$  errors.

The interpretation of naive mean square fit errors must however be taken with caution: In real space the tail of the correlation function dominates the scattering coefficient while absolute values are very small, thus having a low influence on the fit error. This also prevents a direct comparison of fit metrics between real space models and Fourier models (like SHS). For SHS, Fig. 10 however visually reveals that the fit is poor, in particular for low  $k$  values. The difficulties of fitting the SHS sphere model to micro-CT data is well-known [14] and remains here the main reason for the poor performance of the SHS model. The comparison reveals that the details of the retrieval of microstructure parameters from CT or thin section image data are a critical, non-trivial problem that extends beyond the scope of this article. Implications and future work are indicated in the discussion.

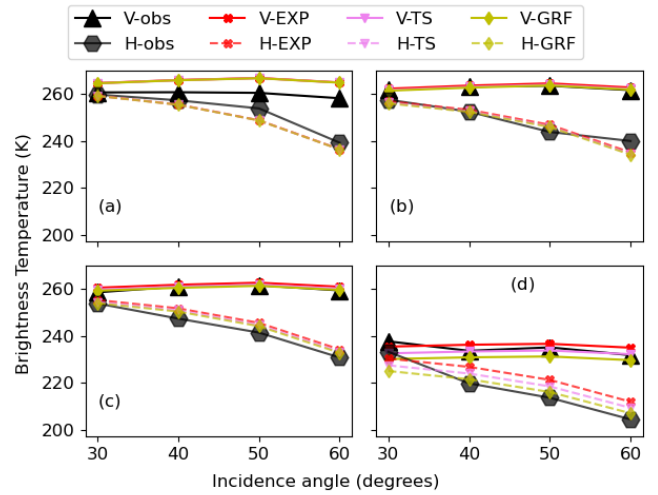


Fig. 11. Brightness temperature variation with incidence angle for NoSREx experiment on Mar. 1, 2012. (a) 10.65 GHz, (b) 18.7GHz, (c) 21 GHz, and (d) 36.5 GHz.

#### D. Complex Snowpack (NoSREx)

The NoSREx data provide an opportunity to evaluate SMRT for a deeper, more complex snowpack with soil substrate and a range of incidence angles. Fig. 11 shows the angular dependence of  $T_B$  for the EXP, TS and GRF models as these demonstrated the smallest errors in Table II. The difference between simulations for each microstructure model increased with increasing frequency. All three microstructure models agreed well with observations, with RMSE between 3.1 and 4.3 K, and all simulations generally followed the observed shape of the brightness temperature curves. At 21 and 36.5 GHz,  $T_B$  at H-pol were overestimated at incidence angles of 40° and larger.

The polarization difference at 10.65 GHz is too large for all microstructural models, which is an indication that the layer thicknesses could be too thin [34]. Layer thicknesses of 2.37 mm were taken directly from the resolution of the micro-CT data, but are actually smaller than the wavelength (28 mm). Resampling of the stratigraphic EXP microstructural properties from 320 to 16 layers of thickness 47.45 mm is

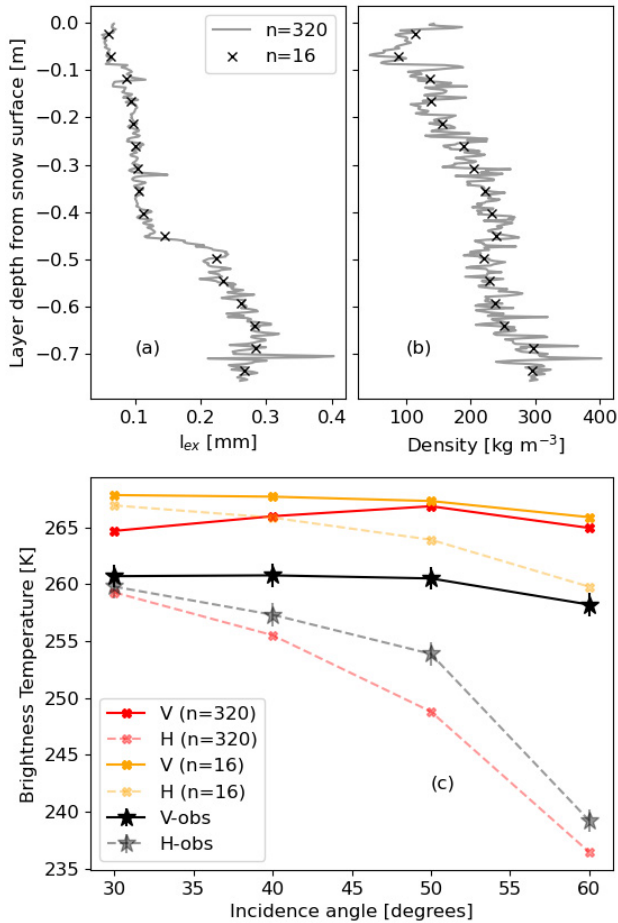


Fig. 12. Impact of changing stratigraphic resolution of (a) exponential correlation length and (b) density on (c) 10.65 GHz  $T_B$  curves. High resolution (HR) simulations have 320 layers whereas low resolution (LR) have 16 layers.

illustrated in Fig. 12(a) and (b). Resampling captured the trend in density and exponential correlation length, but not the high densities and exponential correlation lengths observed in some thin layers at the base of the snowpack. The effect of lower resolution stratigraphy on simulated  $T_B$  at 10.65 GHz is shown in Fig. 12(c). Both H- and V-pol  $T_B$  increased, with a greater impact at H-pol. This narrowed the polarization difference, but at the cost of  $T_B$  simulation accuracy.

### E. Backscatter

Simulations of total backscatter ( $\sigma_0$ ) with the lower resolution NoSREx snowpack are shown in Fig. 13. No observations were made of the bare soil backscatter ( $\sigma_s$ ), so the relative accuracy of the simulations is linked to the chosen parameterization of  $\sigma_s = -13$  dB. Consequently, no error metrics have been presented and it is not possible to conclude any one microstructure model is a better representation than any other. These simulations are intended to highlight differences (or lack of differences) between microstructure models over a range of incidence angles.

As with the passive simulations, microstructure model differences shown in Fig. 13 are greater at higher frequencies.  $\sigma_0$  was highest for the TS model (closely followed by GRF), and lowest for the SHS microstructure model. At 16.7 GHz

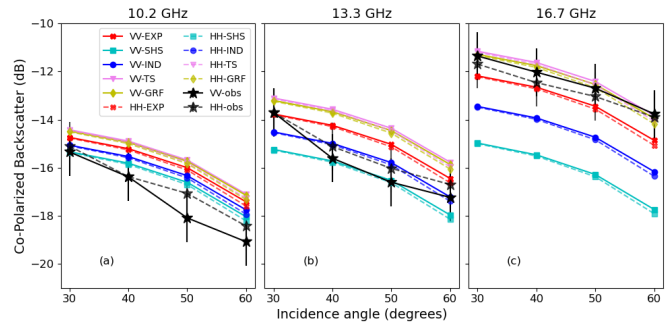


Fig. 13. Comparison between SMRT simulated backscatter and NoSREx observations on Mar. 1, 2012. Panels (a)–(c) show copolarized backscatter, whereas panels (d)–(f) show cross-polarized backscatter. 1 dB measurement error shown.

and incidence angle of  $50^\circ$ ,  $\sigma_0$  for TS microstructure was  $-12.4$  dB, but  $-16.3$  dB for SHS microstructure. Differences between VV and HH  $\sigma_0$  were smaller in the simulations than observations, with a larger decrease in HH  $\sigma_0$  with incidence angle than for VV. At 10.2 and 13.3 GHz observed HH  $\sigma_0$  was higher than VV  $\sigma_0$ , whereas at 16.7 GHz, VV  $\sigma_0$  is higher than HH  $\sigma_0$ . For all simulations, VV  $\sigma_0$  is higher than HH  $\sigma_0$ . Cross-polarization simulations have not been presented as SMRT does not currently account for cross-polarization backscatter contribution from the substrate.

Copolarized backscatter behavior is broadly captured by SMRT, but the difference between microstructure models can exceed measurement error. No conclusions can be drawn as to the most appropriate microstructure for these data due to uncertainty in the soil backscatter contribution. Improved knowledge of substrate reflectivity is key to demonstrating simulation accuracy.

## V. DISCUSSION

SMRT accuracy in this study is comparable to or better than other studies, but the main improvement is that it is achieved without *ad hoc* scaling or optimization of microstructure parameters. The snow parameters are purely based on *in situ* measurements. Evaluation of SMRT against these data shows the largest RMSE for the ASMEEx dataset and the smallest for NoSREx. ASMEEx RMSE errors are similar to those found in [18], where mean RMSE in the frequency range 19–89 GHz for both Arctic and Sub-Arctic snow was 16 and 23 K for EXP and SHS microstructure, respectively. While RMSE is comparable for ASMEEx, the ME is lower than in [18]. Studies with other microwave emission models indicate mean RMSE (19–37 GHz) of around 13 K [10] and 16–26 K [12], but as with [18], these were based on microstructure optimization techniques not applied here. Improvements in SMRT simulations come from the ability to determine and use microstructural parameters directly from micro-CT or thin section images, and from new microstructural models available in SMRT.

Precisely how microstructure parameters are derived requires further attention in a number of areas: 1) fit technique, 2) anisotropy, and 3) stratigraphy. The current method used to fit the analytical microstructure models to the measured correlation function places no weight on different portions of

the curve, meaning fits can be worse at length scales more relevant to particular frequencies.

SHS cannot easily be compared with other microstructure models because the fit to micro-CT data must be done in Fourier space. SHS did not perform well for PAMIR and NoSREx, yet has the potential to perform well as shown by ASMEEx. It is difficult to retrieve parameters for the SHS model [14] as the retrieval tends to identify the lowest possible stickiness as shown in Table I. The fit of the SHS correlation function to experimental data is subject to degeneracy: similar goodness of fits can be obtained by simultaneous variation of diameter and stickiness. For PAMIR, fits to the correlation function at low  $k$  are relatively poor and these parameters are likely more representative at higher frequencies. Microstructure models that have both real-space and Fourier-space analytical correlation functions (IND, EXP, TS) could be used to provide insight into fitting methodology e.g., whether better results can be obtained by fitting in Fourier space. This would also allow us to assess whether it is advantageous to perform the orientational averaging of anisotropic snow in real or Fourier space.

Anisotropy has been demonstrated here, even in snow that visually appears homogeneous, and snow with predominantly vertical structures is simulated less well. The simple assumption applied here was that the isotropic parameters currently required in SMRT could be represented by an equally weighted average of microstructure parameters derived along Cartesian directions. As scattering is non-linearly related to microstructure parameters, this may not be the best approach. Non-equal weight given to the microstructural length scales observed in multiple directions could be explored in the first instance and fitting to the directionally averaged correlation function could also be tested, although a fundamental advancement in SMRT may be needed to account for anisotropic media properly.

There are greater differences between microstructure models for PAMIR than for ASMEEx, despite similar snow depths and substrate (absorber). This could be a function of greater snow heterogeneity in the PAMIR experiment than for ASMEEx, but more likely because of generally coarser structures (Table I) enhancing the sensitivity to microstructure. PAMIR provides interesting data. In this study, ice lenses were not treated as separate thin layers, so there is potential to improve simulations further through explicit consideration of coherence and interlayer boundary effects. However, the better performance of TS and GRF compared with other microstructure models within SMRT may mean that the secondary structure parameter is partially able to compensate for coherent and semicoherent effects.

More generally, we need to rethink how we consider snowpack layers. Snow layers for simulations are often defined by the resolution of the field measurements. Micro-CT allows very fine resolution information, potentially at a higher resolution than microwave observations are sensitive to. At 37 GHz the wavelength is 8 mm whereas at 10 GHz it is 30 mm. Since the RT theory is based on energy transport without tracking the wave phase, specification of thinner layers than the wavelength introduces artificial dielectric discontinuities, which leads to overestimated polarization difference in the simulations [34].

SMRT is equipped with a correction for a subwavelength thin layer surrounded by two normal layers, which is relevant for modeling ice lenses, but as with any RT model, SMRT is not able to deal with a snowpack with many layers thinner than the wavelength properly.

PAMIR microstructural parameters were derived from  $\sim 5$  cm sections, which are much larger than the wavelengths of the observations. ASMEEx layers range from 6 mm to 9 mm in thickness: still too fine for the simulations given that the longest wavelength considered is 16 mm. For homogeneous slabs, this would not matter, but vertical bars for simulated  $\kappa_s$  in Fig. 8 indicate a fair degree of variability in many of the slabs. Agreement with retrieved  $\kappa_s$  depends on whether the slabs conform with the retrieval assumptions, but even good simulations of  $\kappa_s$  can lead to poor  $T_B$  simulations if there are more dielectric discontinuities simulated than observed by the sensors. This does not appear to be a problem for the ASMEEx dataset but is for NoSREx at 10 GHz where the layers are thinner and a longer wavelength considered. This only concerns H-pol simulations, particularly at large incidence angles.

Larger micro-CT sampling size allows longer tail correlation function analysis but it is not clear whether layers could then become too large in the simulation and neglect dielectric discontinuities observed by the sensor (e.g., single layer snowpack simulations are generally insufficient) so the question is what is the most appropriate resolution for snowpack stratigraphy? Micro-CT should be used to address this question with the added benefit of informing resolution of future field campaigns to minimize micro-CT processing cost.

Some of the above questions could be addressed by using the measured correlation functions directly in SMRT. This is theoretically possible but needs more understanding of how to prevent numerical instabilities caused by the tail of non-decaying correlation functions. Nevertheless, micro-CT offers the potential to look at microstructure in a way that has not been possible previously and offers a pathway to more accurate simulations. However, field sampling is not as easy as for other microstructural observation methods (e.g., SSA and density), and the laboratory processing to extract the 3-D structure is expensive. More work is needed to speed up the micro-CT processing chain and/or develop strategies for relating field measurable quantities to the microstructural model parameters needed for more accurate simulations.

Accurate quantification of simulation errors is critical for remote sensing applications. For some applications, snow may not be the primary focus but affects the measurements so it is necessary to understand the contribution of snow to the observation error budget in e.g., ice thickness retrievals. In numerical weather prediction, atmospheric observation uncertainty due to snow is an essential requirement for the assimilation of microwave data in lower troposphere sounding channels. SMRT can also be used in the design of future snow monitoring missions for water supply management.

## VI. CONCLUSION

This article evaluated SMRT against three field experiments of differing snowpack complexity and covers a range in

snow type, snow depth, and observation incidence angle. The way snow microstructure is quantified can have a dramatic impact on the simulation of microwave brightness temperature or backscatter and becomes increasingly important at higher frequencies. The optimum microstructure model may depend on snow type, and the new two-parameter TS and GRF microstructure models give more accurate brightness temperature simulations than other microstructure models for two of the three field campaigns evaluated.

At present, micro-CT or thin section images are needed to determine the necessary microstructure parameters. Future research should focus on the following: 1) assess methods to fit microstructure models to micro-CT data 2) how to parameterize microstructure models from field observations, 3) how to treat snowpack layers given that different frequencies observe different dielectric discontinuities, 4) how to account for anisotropy in the microstructure, and (v) quantifying simulation uncertainties in support of remote sensing applications. SMRT provides the framework to do this.

## VII. CODE AVAILABILITY

Code and data to run these simulations are available from [https://github.com/smrt-model/smrt\\_evaluation\\_paper](https://github.com/smrt-model/smrt_evaluation_paper)

## ACKNOWLEDGMENT

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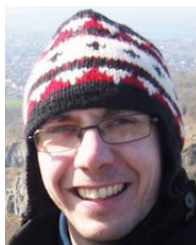
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